



(12) **EUROPEAN PATENT SPECIFICATION**

(45) Date of publication of patent specification :
06.12.95 Bulletin 95/49

(21) Application number : **91102154.1**

(22) Date of filing : **15.02.91**

(51) Int. Cl.⁶ : **H01M 10/12, H01M 10/34,
 H01M 10/10, H01M 4/68,
 H01M 2/02, H01M 2/18,
 H01M 2/12**

(54) **Sealed lead-acid battery.**

(30) Priority : **15.02.90 JP 34611/90
 25.05.90 JP 136077/90
 26.05.90 JP 54924/90 U
 19.06.90 JP 160458/90
 24.10.90 JP 286410/90**

(43) Date of publication of application :
28.08.91 Bulletin 91/35

(45) Publication of the grant of the patent :
06.12.95 Bulletin 95/49

(84) Designated Contracting States :
DE GB IT

(56) References cited :
**GB-A- 787 872
 PATENT ABSTRACTS OF JAPAN, vol. 9, no.
 277 (E-355)[2000], 06 November 1985**

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EP 0 443 451 B1

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Description**BACKGROUND OF THE INVENTION**

5 This invention relates to an improvement in sealed lead-acid batteries.

Sealed lead-acid batteries that make use of a phenomenon called "oxygen cycle" (i.e. oxygen gas evolved during charging is absorbed by the negative electrode) are available in two types, a retainer-type and a gel-type. In a retainer type sealed lead-acid battery, a mat separator (glass separator) made of fine glass fibers is inserted between a positive and a negative plate in order to retain the necessary amount of sulfuric acid electrolyte for charging and discharging the battery and for keeping the electrodes apart. The retainer-type battery has many advantages such as maintenance-free operation, no electrolyte leakage and attitude independence. Consequently, this battery has recently been used in increasing volume as a power source for portable equipment, cordless convenience devices and computer backups. The glass separator used in retainer-type sealed batteries is a mat of very fine glass fibers of a diameter of approximately 1 micron or less, which are made by a special technique. Therefore, the separator is considerably more expensive than separators in common use with lead-acid batteries. Furthermore, in order to attain the desired battery performance, an assembled element must be compressed into a container with great force, which makes the assembly of a battery difficult and unavoidably increases the cost of battery production. Another problem with retainer type sealed lead-acid batteries is that sulfuric acid electrolyte is only retained in the glass separator inserted between positive and negative plates, so less electrolyte can participate in the charge and discharge cycles. Compared to open type common lead-acid batteries, the capacity (in particular the low-rate discharge capacity) of the retainer-type ones is low because sulfuric acid used in lead-acid batteries is one of the active material and the battery capacity is limited by the amount of electrolyte. The positive and negative plates in retainer-type sealed lead-acid batteries are usually made of grids of antimony-free lead alloy having high hydrogen overvoltage. Repeated "deep" charge and discharge cycles of these batteries forms a passivated layer of poor conductivity at the interface between the positive grid and the positive active material, leading to premature loss of the battery capacity. This phenomenon can be prevented by using the positive grid of a lead alloy containing a small amount of antimony. However, the addition of antimony lowers the hydrogen overvoltage and increases the amount of water loss during charging to such an extent that the life of the battery is exhausted prematurely and the batteries dry up, which is fatal to sealed lead-acid batteries. Hence, it has been impossible to use antimony-containing lead alloys in sealed lead-acid batteries that make use of an oxygen cycle. Compared to the retainer-type, gel-type lead-acid batteries are inexpensive but their life performance has been lower than the retainer-type and open type common lead-acid batteries that use a sufficient amount of electrolyte.

35 **SUMMARY OF THE INVENTION**

The present invention has taken into consideration these inadequacies and has as its object to provide an inexpensive sealed lead-acid battery having improved battery performance in which a powder having a higher porosity and a larger surface area than active materials in lead-acid batteries is directly placed between electrode plates and around the assembled element. The necessary amount of sulfuric acid electrolyte for charging and discharging the battery is retained in the powder.

A BRIEF DESCRIPTION OF THE DRAWINGS

45 Fig. 1 is a schematic view of a sealed lead-acid battery according to an embodiment of the present invention;
 Fig. 2 is a schematic view of a sealed lead-acid battery according to another embodiment of the present invention;
 Figs. 3 and 4 are schematic views of two examples of the separator that can be used in the sealed lead-acid battery of the present invention;
 50 Fig. 5 illustrates a method by which the porous material to be used in the sealed lead-acid battery of the present invention is inserted into a container;
 Fig. 6 illustrates the sealed lead-acid battery of the present invention with its outer wall container being enforced with rigid plates;
 55 Fig. 7 is a characteristic diagram showing the antimony adsorbing capability of the powder used in the sealed lead-acid battery of the present invention; and
 Fig. 8 is a characteristic diagram showing the life performance of the sealed lead-acid battery of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

Glass separators commonly used in retainer-type sealed lead-acid batteries are in mat form which have specific surface areas of 1 - 2 m²/g and porosities of about 90%. The greater part of the pores present are about 10 microns in size. Therefore, if the powder which is packed in a container that accommodates an assembled element, has characteristics comparable to glass separators, it should be capable of retaining the necessary amount of sulfuric acid electrolyte for charging and discharging the battery. In addition, the powder can also be placed around the assembled element, so more electrolyte can be retained than in the conventional retainer-type sealed lead-acid batteries. This promises potential improvement in battery performance. Furthermore, the need to compress the assembled element as in the retainer-type sealed lead-acid batteries is eliminated to facilitate the assembly of a battery.

In order that a powder can be used in place of glass separators commonly used in retainer-type sealed lead-acid batteries, it must have a sufficiently high porosity and large specific surface area to retain sulfuric acid electrolyte in a necessary and sufficient amount for charging and discharging the battery. Sealed lead-acid batteries which make use of an oxygen cycle require oxygen gas evolved at the positive electrode to diffuse to the negative electrode where it is absorbed. Thus channels which allow the passage of oxygen gas there through, must be formed in the layer of a powder in a closely packed condition. In order to attain a high specific surface area, a powder is used, which includes the finest possible particles. However, the interstices formed from the densely(closely) packed particles are so small that sulfuric acid electrolyte impregnated within the powder will completely fill those interstices leaving no gas channels behind. This prevents the progress of the reaction required to cause adequate absorption of the oxygen gas. Conversely, if the primary particles in the powder are coarse, the interstices between them are large thereby favoring the formation of gas channels. However, coarse powder includes small specific surface areas and are not able to retain the necessary amount of electrolyte. Under these circumstances, the present invention uses a powder comprising coarse secondary particles that are agglomerates of fine primary particles, whereby sulfuric acid electrolyte is retained by the fine primary particles in a necessary and sufficient amount for charging and discharging the battery so as to insure a smooth cell reaction. In addition, the interstices formed between closely packed coarse secondary particles are used as gas channels to permit an efficient reaction for oxygen absorption.

An example of a powder that possesses these characteristics is hydrous silicon dioxide (SiO₂·nH₂O), which may be prepared either by a wet method involving decomposition of sodium silicate with hydrochloric acid or sulfuric acid, or by a dry method involving the burning of a silicon halide. Hydrous silicon dioxide is an inexpensive industrial material that is generally called "white carbon". While powders in this class have various particulate forms depending on the method of preparation, all of them are highly acid resistant and hydrophilic and consist of very fine primary particles. The primary particles have a diameter of 5 - 40 milli-microns and a specific surface area of 20 - 400 m²/g. Usually, these fine particles agglomerate to form secondary particles of 10 - 500 microns, providing a porosity of 85 - 90% for the powder when it is in a packed condition. The present invention has additionally discovered that the powder described above had a noteworthy characteristic, namely the high ability to adsorb antimony. The present invention is described below in detail with reference to a working example.

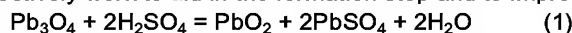
Example

Fig. 1 is a schematic view of the sealed lead-acid battery of the present invention. A positive plate indicated by 1 is a grid made of an antimony-free lead alloy or a low antimony lead alloy (i.e., an alloy containing a small amount of antimony) and which is filled with a positive paste. An antimony-free lead alloy can be selected from common lead-calcium alloys containing 0.02 - 0.12 wt% Ca and 0.20 - 1.0 wt% Sn. For consistent casting of the positive grid, the addition, of 0.001 - 0.01 wt% aluminum is preferred because it prevents the oxidative loss of calcium in the melt. As noted above, the hydrous silicon dioxide powder used as an electrolyte retainer has the ability to absorb antimony, and thus antimony containing lead alloys can be used. Fig. 7 shows the results of an experiment conducted to investigate how much antimony could be adsorbed on the hydrous silicon dioxide powder.

The experimental procedure is set forth hereafter. Varying concentrations of antimony were dissolved in dilute sulfuric acid to prepare solutions (100 ml) with a specific gravity of 1.30. To each solution, 5 g of a hydrous silicon dioxide powder comprising primary particles with a diameter of 10 - 40 millimicrons and having a specific surface area of 120 m²/g was added. The mixtures were agitated with a magnetic stirrer at room temperature for 24 hours and the concentration of antimony in the supernatant was measured. The amount of antimony adsorbed on the hydrous silicon dioxide powder was determined from the difference between the antimony concentration of a blank solution and the concentration of antimony in each test solution. The amount of an-

timony adsorption on the hydrous silicon dioxide powder increased with the concentration of antimony in the solution and at antimony concentrations of 50 mg/L and above, one gram of the powder adsorbed 2.0 mg and more of antimony. This was higher than the antimony adsorption on rutile type titanium dioxide and β -form lead dioxide which are good antimony adsorbents. The antimony adsorption was dependent on the specific surface area of the hydrous silicon dioxide powder, which was capable of good antimony adsorption at values of 100 m²/g and above. These results show that antimony-containing lead alloys could be used in the positive grid as effectively as antimony-free lead alloys since antimony released from the positive electrode was trapped before it reached the negative electrode without lowering the hydrogen overvoltage. It should however be noted that the amount of antimony added is preferably as small as possible while still remaining sufficient to attain the intended effect of antimony. Hence, antimony is preferably added in an amount of 0.7 - 2.0 wt%, with the range of 0.7 - 1.2 wt% being particularly preferred. Antimony, arsenic (As) and tin (Sn) may be added in respective amounts of 0.1 - 0.3 wt% and 0.01 - 0.5 wt%. If selenium (Se) or sulfur (S) is added in very small amounts as a nucleating agent, the castability and corrosion resistance of the grid can be improved.

The paste which is applied to the positive grid may be any common positive paste, which is prepared by mixing a lead oxide powder with dilute sulfuric acid. More preferably the lead oxide powder is mixed with red lead (Pb₃O₄) to aid in the step of electrochemically forming the positive plate and to improve the battery performance. Red lead reacts with sulfuric acid in accordance with the following equation (1) and the resulting lead dioxide (PbO₂) will effectively work to aid in the formation step and to improve the battery performance:



However, if a lead oxide powder is merely mixed with red lead before dilute sulfuric acid is added for mixing, PbO₂ will not form. This is because the reaction expressed by the following equation (2) will proceed at a faster rate than the reaction of eq. (1), causing the added sulfuric acid to be consumed by the lead oxide (PbO) in the lead oxide powder:



Hence, in order to form lead dioxide during the paste mixing process, it is recommended that dilute sulfuric acid be first added to red lead so as to initiate the reaction of eq. (1), with a lead oxide powder being subsequently added, followed by further mixing. In this way, lead dioxide will be formed in the amount calculated from eq. (1), whereby the quantity of electricity necessary to electroform the battery is reduced and the battery performance is improved. To this end, red lead must be used in an amount of at least 20 wt% of the weight of the lead oxide powder.

A negative plate indicated by 2 in Fig. 1 is fabricated by pasting a grid of antimony-free lead alloy with a common negative paste incorporating an expander agent such as lignin and/or barium sulfate. The lead alloy as the material for the negative grid may be selected from among common lead-calcium alloys containing 0.02 - 0.12 wt% Ca and 0.001 - 0.5 wt% Sn.

The positive and negative grids described above can be manufactured by various methods such as by casting, punching sheets of lead alloys and by the expanded metal process. The pasted grids are used as electrode plates after curing in a room at 30 - 50 °C. The curing of positive grids is a particularly important step for battery performance.

A synthetic separator 3 is inserted between the positive and negative plates. Any separator can be used as long as it is as thin as 0.02 - 0.3 mm, has a porosity of 70 - 80% and exhibits low electric resistance. Separators having pores of diameter of less than 1 micron are not preferred, since they are not highly permeable to gases. A plurality of projections 4 or 4' are provided on one or both sides of the separator 3 as shown in Fig. 3 or 4. In a sealed lead-acid battery of the type contemplated by the present invention which uses a powder as an electrolyte retainer, the powder must be packed evenly between the positive and negative plates. The projections are provided in order to keep the plates apart by a constant distance and can be easily formed by depositing, with a hot-melt gun, a molten resin in dots or in discontinuous lines on a strip sheet used for separation, which is unwound from a roll. In areas where projections are formed, pores in the separator will be blocked to cause the loss of ion conductivity. Hence, allowing the projecting areas to occupy an unduly large space is not preferred, since it would hinder battery performance. The projecting areas should not occupy more than 1% of the total area of the separator. Under these circumstances, small projections are preferably distributed over the surface of the separator in order to keep the positive and negative plates apart by a constant distance. In the present example, a synthetic separator having a thickness of 0.25 mm, a porosity of 73% and an average pore diameter of ca. 4 microns was provided on one side with a plurality of projections each having a diameter of ca. 2 mm and a height of 1.2 mm in such a way that their total area occupied ca. 0.7% of the separator surface.

The positive plates, negative plates and the separators provided with projections are stacked and assembled into an element, with the individual positive plates being soldered separately from the negative plates. The assembled element is then inserted into a container 5. Whereas, the conventional element, which uses

glass separators, experiences considerable difficulty when inserting the separator into a container unless the element is compressed with great force. However, in the present invention, there is no need to compress the assembled element and it can be easily inserted into the container. After inserting the element, a powder 8 is packed both between the plates and around the element. In the example being discussed, the powder comprises fine primary particles of hydrous silicon dioxide diameters of 10 - 40 millimicrons and specific surface areas of 100 - 150 m²/g. The primary particles agglomerate to form secondary particles with diameters of 50 - 200 microns. This powder is highly flowable and has an angle of repose of 25 - 30 degrees. Having such high fluidity, the powder can be closely packed into the container within a short time by applying vibrations with an amplitude of 1 - 2 mm under an acceleration of gravity of 2 - 4 g. The powder 8 is placed in such a way that a positive strap 6 and a negative strap 7 are just covered.

A porous layer 9 covers the top of the layer of packed powder 8. As already mentioned, the powder used in the present invention has such high fluidity that unless its layer is immobilized with the porous layer 9, the particles of the powder will readily move to create voids in its layer. These voids are especially created when sulfuric acid electrolyte is added to an uncharged battery or during gassing in the initial charge. Voids in the layer of powder are unable to retain the electrolyte and the active materials will not work effectively to attain the desired battery performance. Hence, immobilizing the layer of powder is very important. The porous layer 9 may be made of any porous material that is permeable to liquids and gases but which is impervious to the particles of the powder. Needless to say, the porous material must resist sulfuric acid without releasing any deleterious materials. A suitable example of such porous materials is a foamed phenolic resin. Foamed phenolic resins are highly acid-resistant and have sufficient strength although they are somewhat brittle. If a rectangular block 9' of phenolic resin foam that is slightly larger than the size of the container as shown in Fig. 5 is pressed against the top end of the container 5, it is cut by the edge of the top lateral sides of the container and its partitions. Thus, the block can be inserted into several cells of the container simultaneously. If small holes 10' are made in the block of phenolic resin foam in positions that correspond to cell posts 10, the latter will penetrate just snugly through the holes as the block is forced into the container. The phenolic resin foam is also snugly fitted over an inter-cell connector 11 by concaving in a corresponding shape. The porosity of the phenolic resin foam can be easily changed by adjusting the blow ratios. Experimental results show that blow ratios of 10 - 100 are appropriate. After accommodating the assembled element into the container and filling it with the powder which is then immobilized with the porous material, a cover 12 is bonded or soldered to the container 5 to complete an uncharged battery. The cover 12 has a vent plug 13 as an integral part and a vent valve 14, which will open when the pressure in the battery rises and close when the pressure decreases. The vent valve 14 may be of any common type such as a cap valve, a ring valve or a plate valve. The vent valve may be fitted either after filling the uncharged battery with sulfuric acid electrolyte or after the initial charging. In the latter case, the valve must be fitted immediately after initial charge is completed.

The electrolyte retainer used in the sealed lead-acid battery of the present invention is a powder having high fluidity as described above, and thus voids are prone to form in the layer of that powder under the pressure of gases evolved during initial charging of the battery. To avoid this problem, the powder 8 is immobilized with the porous layer 9 but, even then, the evolution of gases during charge is preferably as small as possible. The positive paste used by the present invention contains lead dioxide in the unformed active material and a smaller quantity of electricity enables the battery to be charged, whereby the problem described above can reasonably be prevented. Consider, for example, a sealed lead-acid battery having a 5-h rate capacity of 24 Amp-hours (Ah). With batteries using the conventional positive paste, electricity of 160 - 180 Ah is necessary for charging. However, 80 - 120 Ah is sufficient to charge the battery of the present invention. Since the quantity of charging electricity is reduced, less water will be electrolyzed during charging, thereby minimizing the evolution of gases. Needless to say, a smaller amount of sulfuric acid is needed within the uncharged battery. This feature can be utilized to enable the manufacture of compact batteries.

Fig. 2 shows a sealed lead acid battery according to another embodiment of the present invention, in which the porous layer 9 is placed below the vent plug 13 and the vent valve 14 is placed above the plug 13 in order to reduce the space in the upper part of the battery. In this embodiment, the container 5 accommodating the assembled element is fitted with the cover 12 by either bonding or soldering and then the powder 8 is fed into the container through the port where the vent plug 14 is to be fitted, followed by the fitting of that plug. The electrolyte is added with the vent valve 14 removed, which is fitted either after the addition of electrolyte or after charging the battery. In the embodiment shown in Fig. 2, the head space of the battery is sufficiently reduced to improve the volume energy efficiency of the battery by at least ca. 20%.

As is well known in the art, upon repeated charge and discharge, the thicknesses of electrode plates in a lead-acid battery will expand gradually due to the volume change of the active materials and the corrosion of the grids. The glass separators used in conventional retainer-type sealed lead-acid batteries have no rigidity, so the stress due to expansion of the plates is absorbed by the glass separators, thus preventing the container

wall from deforming. On the contrary, the glass separators immersed in sulfuric acid electrolyte will lose elasticity. Therefore, to maintain the force by which the assembled element is compressed, it is necessary to assemble the battery with the element being preliminarily compressed with adequate force. This is why it has been difficult to assemble conventional retainer type sealed lead-acid batteries. In contrast, the powder used as an electrolyte retainer in the sealed lead-acid battery of the present invention has a low compressibility characteristic, so the stress due to expansion of the plates will be directly applied to the container wall, eventually causing it to deform outward. This deformation is particularly great if the battery is used at high ambient temperatures, which decreases the strength of the synthetic resin used to make the container wall. The plate expansion in the sealed lead-acid battery of the present invention exerts enough stress to deform the container wall. Therefore, a great compressive force is applied to the assembled element as reinforcement to permit the battery to exhibit superior life performance. When the container wall is reinforced against deformation, plate deterioration is suppressed to further prolong the life of the battery. Two possible ways to prevent the deformation of the container wall is by using high-strength materials for the container or by increasing the thickness of the container wall. However, these methods will increase either the weight or the cost of the battery. A convenient alternative method is to improve the battery's carrier as in automotive applications by attaching reinforcing rigid plates to container wall surfaces that are parallel to the electrode plates in the battery as shown in Fig. 6. Numeral 15 denotes the sealed lead-acid battery of the present invention, and 16 and 16' are the reinforcing plates made of iron or aluminum that are fixed to the container wall by means of bolts 17 and nuts 18.

The sealed lead-acid battery of the present invention was subject to an initial performance test and a life test and the results are described below. The test samples were 12 V automotive sealed lead-acid batteries with a nominal capacity of 25 Ah. The specifications of the batteries being tested are shown in Table 1.

TABLE 1

Sample	Alloy of Positive Grid	Electrolyte Retainer	Remarks
A	Pb-0.10%Ca -0.70%Sn	powder	invention
B	Pb-1.0%Sb -0.2%As -0.2%Sn	powder	invention
C	Pb-0.10%Ca -0.70%Sn	glass separator	prior art
D	Pb-1.0%Sb-0.2%As -0.2%Sn	glass separator	prior art

Samples A and B were batteries of the present invention using a powder as an electrolyte retainer; sample A used a lead-calcium alloy in the positive grid and sample B used a lead-antimony alloy. Samples C and D were prior art batteries using a lead-calcium and a lead-antimony alloy, respectively, in the positive grid. In each test sample the negative grid was made of a lead-calcium alloy (Pb-0.7% Ca-0.5% Sn). Needless to say, the positive plates in the samples of the present invention were made from a paste that was prepared by mixing a leady oxide powder with 30% red lead to the recipe described herein. The content of lead dioxide in the paste was found to be 5.9 wt%. The batteries of the present invention could be charged with about 40% less electricity than the prior art batteries required. The charged batteries were subjected to a 5-h rate discharge test and a 150 A discharge test at -15°C. The life test was conducted primarily for the purpose of evaluating battery performance at elevated temperatures. This test was a constant-voltage life test at 75°C which was higher than the normal operating temperature. The test conditions are shown specifically below:

Ambient temperature : 75°C
 Discharge : 4 min at 25 A
 Charge : 10 min at 14.8 V
 (maximum current = 25 A).

The results of the initial performance test are shown in Table 2 and those of the life test in Fig. 8. Also subjected to the life test was battery B' which was the same as B except that the container wall was reinforced with synthetic resin laminated steel plates as shown in Fig. 6.

TABLE 2

Sample	5-h rate capacity	150 A discharge test at -15°C
A	27. 7 Ah	8. 6 Ah (9. 40V)
B	28. 5	8. 7 (9. 20)
C	25. 2	7. 5 (9. 40)
D	24. 0	7. 0 (9. 20)

*Figures in parentheses indicate 5-sec discharge voltages.

The initial performance of samples A and B of the present invention was ca. 10% better than prior art samples C and D in terms of both 5-h rate capacity and 150 A discharge capacity. This would be because the samples of the present invention could retain electrolyte ca. 20% more than the prior art samples and because the incorporation of red lead into the positive paste improved the formability of the positive plates.

At every 500 charge and discharge cycles under the life test conditions described above, each battery was discharged at a cold cranking current (274 A) for the 30-sec and the life test was completed when the battery failed to maintain 7.2 V (1.2V/cell) for 30sec. The determined battery life was 1,800 cycles for sample A, 2,600 cycles for sample B and 3,500 cycles for sample B'. These results were superior to the prior art samples C (1,400 cycles) and D (800 cycles). In particular, sample B which used a lead-antimony alloy in the positive grids exhibited life performance over three times as long as the life of prior art retainer-type sealed lead-acid battery D using the same alloy. Sample B' in which the container wall was reinforced with steel plates had an even longer life (3,500 cycles). The water loss during the life test was determined by measuring the weight of each battery at every 500 cycles. The amount of water loss is a measure for the recombination efficiency of a sealed lead-acid battery. In samples A and C using a lead-calcium alloy in the positive grids, the volume of electrolyte decreased at substantially the same rate and the water loss per se was comparatively small. The positive grids in sample B and B' which used a hydrous silicon dioxide powder as an electrolyte retainer in accordance with the present invention were made of a lead-antimony alloy and yet the water loss was just a bit greater than in samples A and C which used antimony-free positive grids. On the other hand, lead-antimony alloy in the positive grids, experienced a marked increase in a water loss due to an increased current at the end of charge. This is because antimony released from the positive grids precipitated at the negative plates, whereby the hydrogen overvoltage dropped to increase the chance of water electrolysis. This would be one of the reasons why the life of prior art battery D was extremely short. In comparison, samples B and B' of the present invention, which used a hydrous silicon dioxide powder as an electrolyte retainer, were capable of preventing the drop of hydrogen overvoltage at the negative plates, since antimony released from corroded positive grids was effectively trapped by the powder before it reached the negative plates. As a result, the water loss due to water electrolysis decreased and, combined with the better corrosion resistance of the positive grids than those made of an antimony-free alloy. This effect contributed superior life performance to samples B and B'. Examination after the life test revealed slight expansion in the container walls of sealed lead-acid batteries A and B of the present invention. However, battery B' in which the container wall was reinforced with steel plates did not deform at all. Inspection after disassembly showed that prior art sealed lead-acid batteries C and D using glass separators experienced heavy corrosion at the positive grids. In particular, the positive plates in battery C using antimony-free grids deteriorated to an unidentifiable form. In contrast, the electrode plates in the batteries of the present invention were firmly secured by the hydrous silicon dioxide powder packed into the container and they experienced only small deformation. The extent of electrode deformation was particularly small in battery B' which of electrode deformation was particularly small in battery B' which had the container wall reinforced with steel plates. This would be another reason for the superior life performance of the batteries of the present invention.

As described above, the sealed lead-acid battery of the present invention is based on two new concepts for sealed lead-acid batteries. These concepts include retaining an electrolyte by fine primary particles having a large specific area and creating interstices from relatively coarse secondary particles formed by agglomeration of those primary particles which are closely packed together and used as gas channels. This battery

exhibits better performance and oxygen absorbing reactions than conventional retainer-type sealed lead-acid batteries using glass separators. In addition to the hydrous silicon dioxide powder, the electrolyte retainer for use in the sealed lead-acid battery of the present invention may be made of any powder such as one of tabular crystals of calcium silicate ($\text{CaO} \cdot 2\text{-}2.5\text{SiO}_2 \cdot \text{H}_2\text{O}$) that has acid resistance and hydrophilicity and which comprises fine primary particles have a large specific surface area and a high porosity that will agglomerate to form coarse secondary particles. If the secondary particles in the powder are friable, a suitable binder may be used. According to another discovery of the present invention, the hydrous silicon dioxide powder has the ability to easily adsorb antimony. This characteristic enables the use of antimony containing grids that have been impossible to use in conventional sealed lead-acid batteries. The result is a marked improvement in the life performance of the battery of the present invention. Furthermore, the absence of the need to compress the assembled element facilitates cost. In conventional retainer-type sealed lead-acid batteries, negative plate lugs and strap are exposed, so when the battery is used under adverse conditions such as high temperature and overcharge, the lugs and strap will corrode, occasionally leading to a critical accident such as explosion of the battery. However, in the sealed lead-acid battery of the present invention, the assembled element is totally embedded in the layer of the powder specified herein. The negative plate lugs and strap will not corrode even if the battery is used under the adverse conditions described above, which is one of the major advantages of the present invention.

While a typical example of the present invention has been described above, it may be embodied in various other ways without departing from its scope and spirit. In the embodiment described above, a separator provided with a plurality of small cylindrical or linear projections is inserted between positive and negative plates. But, this separator may be omitted since the powder used in the present invention also has the characteristics of a separator. In this case, a suitable spacer is inserted between the plates to keep them apart, with the powder as an electrolyte retainer being placed both between the plates and around the assembled elements. A fairly large space must be allowed between the plates in order to prevent shorting. Experimental results showed that the space had to be at least about 1.5 mm. Secondly, a tubular sealed lead-acid battery can easily be manufactured by application of the present invention. Conventionally, glass separators cannot be used in tubular lead-acid batteries since the positive plates are not flat and this has inevitably led to the manufacture of short-lived gel-type sealed batteries. This serious drawback is eliminated by the present invention which enables a tubular sealed lead-acid battery of superior life performance to be manufactured by a simplified process.

While various embodiments have been chosen to illustrate the present invention, it will be understood by those skilled in the art that various changes and modifications can be made therein without departing from the scope of the invention as defined in the appended claims.

Claims

1. A sealed lead-acid battery with a vent valve comprising:

a container (5) accommodating an assembled element comprising:

- at least one electrochemically formed positive plate (1) having a grid of an antimony-free alloy pasted with a porous active material;
- at least one electro-chemically formed negative plate (2) having a grid of an antimony-free lead alloy pasted with a porous active material, and a separator (3) inserted between said positive and negative plates (1, 2), said separator (3) having a plurality of projections (4, 4') on one or both side thereof;
- a layer of powder placed between said positive and negative plates (1, 2) and around said assembled element, said powder layer being composed of a closely packed powder (8), which is acid-resistant and hydrophilic and which has a higher porosity and a larger specific surface area than said active materials, said powder layer having interstices in its interior used as gas channels, created when coarse secondary particles formed by agglomeration of fine primary particles are closely packed and being immobilised with an acid-resistant porous layer (9) placed above said powder layer, said porous layer being permeable to gases and liquids, and impervious to particles of said powder layer; and
- sulfuric acid electrolyte impregnated and retained in said positive and negative plates (1, 2) and in said powder layer in a substantially necessary and sufficient amount for charging and discharging the battery.

2. The sealed lead-acid battery according to claim 1, wherein the electrolyte necessary for charging and discharging the battery is substantially retained by said fine primary particles in said powder layer and wherein oxygen gas, evolved at the positive electrode (1) during charging, is absorbed through said gas

channels by the negative electrode (2), said battery utilising an oxygen cycle involving no free electrolyte.

3. The sealed lead-acid battery according to claim 2, wherein said powder layer used as an electrolyte re-
 5 tainer contains as a main component hydrous silicon dioxide ($\text{SiO}_2 \cdot n\text{H}_2\text{O}$), which comprises fine primary particles with a size of 5 - 40 millimicrons, said primary particles agglomerated to form secondary particles with a size of 10 - 500 microns, said powder layer having a specific surface area of 20 - 400 m^2/g and a porosity of 85 - 90%.
4. The sealed lead-acid battery according to claim 1, wherein said positive plate uses a positive grid made
 10 of an antimony-free lead alloy containing 0.02 - 0.12 wt% calcium, 0.20 - 1.0 wt% tin and 0.001 - 0.01 wt% aluminum and said negative plate uses a negative grid made of an antimony-free lead alloy containing 0.02 - 0.1 wt% calcium and 0.001 - 0.5 wt% tin.
5. The sealed lead-acid battery according to claim 1, wherein said separator is a low-resistance synthetic
 15 separator that has a thickness of 0.02 - 0.3 mm and a porosity of 70 - 80% and which is provided with a plurality of small cylindrical or linear projections on one or both sides thereof.
6. The sealed lead-acid battery according to claim 5, wherein said plurality of small cylindrical or linear pro-
 20 jections that block pores in the separator occupy no more than 1% of the total area of said separator.
7. The sealed lead-acid battery according to claim 5, wherein said small cylindrical or linear projections are
 made of an acid-resistance hot-melt resin.
8. The sealed lead-acid battery according to claim 1, wherein the positive plate is pasted with a paste pre-
 25 pared by mixing a leady oxide powder with red lead in an amount of at least 20 wt% of the leady oxide powder.
9. The sealed lead-acid battery according to claim 8, wherein said positive plate comprises lead dioxide
 30 formed from a mixture of red lead and dilute sulfuric acid and leady oxide powder added to the mixture containing lead dioxide, said mixture being in the form of a paste, which is applied to a positive plate, said positive plate being cured and formed electrochemically.
10. The sealed lead-acid battery according to claim 1, wherein said porous layer is a plate of foamed phenolic
 35 resin that is greater in size than a top face of the container and which has been blown at a ratio of 10 - 100 to produce open cells, said plate being pressed against the top face of the container and forced into individual cells of the battery to immobilize the powder layer packed in the container.
11. The sealed lead-acid battery according to claim 1, wherein said porous layer is placed below a vent plug
 40 and the vent valve is placed above said bent plug in order to immobilize the powder layer packed in the container.
12. The sealed lead-acid battery according to claim 1, wherein rigid plates are attached to outer wall surfaces
 45 of the container parallel to the positive and negative plates in the container, thereby preventing deformation of said outer wall surfaces of the container.
13. A sealed lead-acid battery which a vent valve comprising: a container (5) accommodating an assembled
 element comprising:
 - at least one electrochemically formed positive plate (1) having a grid of a lead alloy containing a small
 amount of antimony, said positive plate (1) being pasted with a porous active material,
 - 50 - at least one electrochemically formed negative plate (2) having a grid of an antimony-free lead alloy
 pasted with a porous active material, and
 - a separator (3) inserted between said positive and negative plates (1, 2), which has a plurality of pro-
 jections (4, 4') on one or both side thereof;
 - a layer of powder placed between said positive and negative plates (1, 2) and around said assembled
 55 element, said powder layer being composed of a closely packed powder (8), that is acid-resistant
 and hydrophilic and which has a higher porosity and a larger specific surface area than said active
 materials, said powder layer having interstices in its interior used as gas channels, created when
 coarse secondary particles formed by agglomeration of fine primary particles are closely packed and

- being immobilised with an acid-resistant porous layer (9) placed on top of said powder layer, and which is permeable to gases and liquids, and which is impervious to the particles of said powder layer; and
- 5 - sulfuric acid electrolyte impregnated and retained in said positive and negative plates (1, 2) and in said layer of powder in a substantially necessary and sufficient amount for charging and discharging the battery.
14. The sealed lead-acid battery according to claim 13, wherein the electrolyte necessary for charging and discharging the battery is substantially retained by said fine primary particles in said powder layer, and wherein oxygen gas, evolved at the positive electrode (1) during charge, is absorbed through said gas channels by the negative plate (2), said battery utilising an oxygen cycle involving no free electrolyte.
15. The sealed lead-acid battery according to claim 14, wherein said powder used as an electrolyte retainer contains as a main component hydrous silicon dioxide ($\text{SiO}_2 \cdot n\text{H}_2\text{O}$) that comprises fine primary particles with a size of 5 - 40 millimicrons which agglomerate to form secondary particles with a size of 10 - 500 microns, said powder layer having a specific surface area of 100 - 400 m^2/g and a porosity of 85 - 90% and being capable of adsorbing at least 2 mg of antimony per gram of said powder.
16. The sealed lead-acid battery according to claim 13, wherein said grid of said positive plate is a positive grid made of a lead alloy containing 0.7 - 2.0 wt% antimony, 0.1 - 0.3 wt% arsenic and 0.01 - 0.5 wt% tin, and said grid of said negative plate is a negative grid made of an antimony-free lead alloy containing 0.02 - 0.12 wt% calcium and 0.001 - 0.5 wt% tin.
17. The sealed lead-acid battery according to claim 13, wherein said separator is a low-resistance synthetic separator that has a thickness of 0.02 - 0.3 mm and a porosity of 70 - 80% and which is provided with a plurality of small cylindrical or linear projections on one or both sides thereof.
18. The sealed lead-acid battery according to claim 17, wherein said plurality of small cylindrical or linear projections that block pores in the separator occupy no more than 1% of the total area of said separator.
19. The sealed lead-acid battery according to claim 17, wherein said small cylindrical or linear projections are made of an acid-resistance hot-melt resin.
20. The sealed lead-acid battery according to claim 13, wherein the positive plate is pasted with a paste comprising a mixture of a leady oxide powder and red lead in an amount of at least 20 wt% of the leady oxide powder.
21. The sealed lead-acid battery according to claim 20, wherein said positive plate comprises lead dioxide formed from a mixture of red lead and dilute sulfuric acid and a leady oxide powder, said mixture forming a paste which is applied to a positive grid, said plate being cured and formed electrochemically.
22. The sealed lead-acid battery according to claim 13, wherein said porous layer is a plate of foamed phenolic resin that is greater in size than a top face of the container and which has been blown at a ratio of 10 - 100 to produce open cells, said plate being pressed against the top face of the container and forced into individual cells of the battery to immobilize the powder layer packed in the container.
23. The sealed lead-acid battery according to claim 13, wherein said porous layer is placed below a vent plug and the vent valve is placed above said vent plug in order to immobilize the powder layer packed in the container.
24. The sealed lead-acid battery according to claim 13, wherein rigid plates are attached to outer wall surfaces of the container parallel to the positive and negative plates in the container, whereby preventing deformation of said wall surfaces of the container.

Patentansprüche

1. Geschlossene Blei/Säure-Batterie mit Entlüftungsventil, welche einen Behälter (5) zur Aufnahme eines

zusammengesetzten Elements umfaßt mit:

- mindestens einer elektrochemisch gebildeten Plusplatte (1) mit einem Gitter aus einer antimonfreien Legierung, die mit einer porösen aktiven Masse pastiert ist;
 - mindestens einer elektrochemisch gebildeten Minusplatte (2) mit einem Gitter aus einer antimonfreien Bleilegierung, die mit einer porösen aktiven Masse pastiert ist, und einem Plattenscheider (3), welcher zwischen der Plusplatte und der Minusplatte (1, 2) angebracht wird, wobei der Plattenscheider (3) eine Vielzahl von Vorsprüngen (4, 4') auf einer Seite oder beiden Seiten aufweist;
 - einer Pulverschicht zwischen der Plusplatte und der Minusplatte (1, 2) und um das zusammengesetzte Element herum, wobei die Pulverschicht aus einem stark verdichteten Pulver (8) besteht, das säurebeständig und hydrophil ist und eine größere Porosität und eine größere spezifische Oberfläche als die aktiven Massen hat, und die Pulverschicht im Innern kleine, als Gaskanäle genutzte Zwischenräume aufweist, die erzeugt werden, wenn durch Anhäufung feiner Primärteilchen entstandene grobe Sekundärteilchen stark verdichtet und mit einer auf die Pulverschicht aufgetragenen säurebeständigen, porösen Schicht (9) unbeweglich gemacht werden, wobei die poröse Schicht gas- und flüssigkeitsdurchlässig und für Teilchen der Pulverschicht undurchlässig ist; und
 - Schwefelsäure-Elektrolyten, mit denen die Plusplatte und die Minusplatte (1,2) sowie die Pulverschicht in einer zum Laden und Entladen der Batterie im wesentlichen erforderlichen und ausreichenden Menge getränkt sind und die in selbigen gehalten werden.
2. Geschlossene Blei/Säure-Batterie nach Anspruch 1, wobei der zum Laden und Entladen der Batterie erforderliche Elektrolyt im wesentlichen durch die feinen Primärteilchen in der Pulverschicht gehalten wird und wobei ein Sauerstoffgas, das sich während des Ladens an der positiven Elektrode (1) entwickelt, durch die Gaskanäle hindurch von der negativen Elektrode (2) absorbiert wird, und wobei die Batterie einen Sauerstoffkreislauf ohne freie Elektrolyte verwendet.
3. Geschlossene Blei/Säure-Batterie nach Anspruch 2, wobei die als Elektrolyt-Haltelement genutzte Pulverschicht als einen Hauptbestandteil ein wasserhaltiges Siliziumdioxid ($\text{SiO}_2 \cdot n\text{H}_2\text{O}$) mit feinen Primärteilchen in einer Größe von 5 - 40 Millimikronen enthält, wobei sich die Primärteilchen zu Sekundärteilchen mit einer Größe von 10 - 500 Mikronen anhäufen und die Pulverschicht eine spezifische Oberfläche von 20 - 400 m^2/g und eine Porosität von 85 - 90 % hat.
4. Geschlossene Blei/Säure-Batterie nach Anspruch 1, wobei die Plusplatte ein positives Gitter aus einer antimonfreien Bleilegierung mit 0,02 - 0,12 Masseprozent Kalzium, 0,20 - 1,0 Masseprozent Zinn und 0,001 - 0,01 Masseprozent Aluminium verwendet und die Minusplatte ein negatives Gitter aus einer antimonfreien Bleilegierung mit 0,02 - 0,1 Masseprozent Kalzium und 0,001 - 0,5 Masseprozent Zinn verwendet.
5. Geschlossene Blei/Säure-Batterie nach Anspruch 1, wobei der Plattenscheider ein synthetischer Plattenscheider mit geringem Widerstand, einer Dicke von 0,02 - 0,3 mm und einer Porosität von 70 - 80 % ist und eine Vielzahl kleiner zylindrischer oder linearer Vorsprünge auf einer Seite oder beiden Seiten aufweist.
6. Geschlossene Blei/Säure-Batterie nach Anspruch 5, wobei die Vielzahl kleiner zylindrischer oder linearer Vorsprünge zum Blockieren der Poren im Plattenscheider nicht mehr als 1 % der Gesamtfläche des Plattenscheiders einnimmt.
7. Geschlossene Blei/Säure-Batterie nach Anspruch 5, wobei die kleinen zylindrischen oder linearen Vorsprünge aus einem säurebeständigen Heißschmelzharz bestehen.
8. Geschlossene Blei/Säure-Batterie nach Anspruch 1, wobei die Plusplatte mit einer Masse pastiert ist, die durch Vermischen eines bleihaltigen Oxidpulvers mit Bleimennige hergestellt wird und letzteres mindestens 20 Masseprozent des bleihaltigen Oxidpulvers ausmacht.
9. Geschlossene Blei/Säure-Batterie nach Anspruch 8, wobei die Plusplatte Bleidioxid umfaßt, welches aus einem Gemisch aus Bleimennige und verdünnter Schwefelsäure gebildet wird, und ein bleihaltiges Oxidpulver dem Bleidioxid enthaltenden Gemisch zugesetzt wird, und wobei das Gemisch die Form einer Paste hat, welche auf eine Plusplatte aufgetragen wird, und die Plusplatte elektrochemisch ausgehärtet und gebildet wird.

10. Geschlossene Blei/Säure-Batterie nach Anspruch 1, wobei die poröse Schicht eine Platte aus Phenolharzschäum ist, die größer als eine Oberseite des Behälters ist und zur Schaffung offener Zellen in einem Verhältnis von 10 - 100 aufgeschäumt wurde, und die Platte gegen die Oberseite des Behälters gepreßt und in die einzelnen Zellen der Batterie eingedrückt wird, um die im Behälter verdichtete Pulverschicht unbeweglich zu machen.
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11. Geschlossene Blei/Säure-Batterie nach Anspruch 1, wobei die poröse Schicht unter einem Entlüftungsstopfen angebracht und das Entlüftungsventil über dem Entlüftungsstopfen angeordnet ist, um die im Behälter verdichtete Pulverschicht unbeweglich zu machen.
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12. Geschlossene Blei/Säure-Batterie nach Anspruch 1, wobei die starren Platten an den Flächen der Behälteraußenwände parallel zu der Plusplatte und der Minusplatte im Behälter befestigt werden, wodurch eine Verformung der Fläche der Behälteraußenwände verhindert wird.
- 15 13. Geschlossene Blei/Säure-Batterie mit Entlüftungsventil, welche einen Behälter (5) zur Aufnahme eines zusammengesetzten Elements umfaßt mit:
 - mindestens einer elektrochemisch gebildeten Plusplatte (1) mit einem Gitter aus einer Bleilegierung, welche eine geringe Menge Antimon enthält, wobei die Plusplatte (1) mit einer porösen aktiven Masse pastiert ist,
 - 20 - mindestens einer elektrochemisch gebildeten Minusplatte (2) mit einem Gitter aus einer antimonfreien Bleilegierung, welche mit einer porösen aktiven Masse pastiert ist, und
 - einem Plattenscheider (3), welcher zwischen der Plusplatte und der Minusplatte (1, 2) angebracht wird und eine Vielzahl von Vorsprüngen (4, 4') auf einer Seite oder beiden Seiten aufweist;
 - einer Pulverschicht zwischen der Plusplatte und der Minusplatte (1, 2) und um das zusammengesetzte Element herum, wobei die Pulverschicht aus einem stark verdichteten Pulver (8) besteht, das säurebeständig und hydrophil ist und eine größere Porosität und eine größere spezifische Oberfläche als die aktiven Massen hat, wobei die Pulverschicht im Innern kleine, als Gaskanäle genutzte Zwischenräume aufweist, die erzeugt werden, wenn durch Anhäufung feiner Primärteilchen entstandene grobe Sekundärteilchen stark verdichtet und mit einer auf die Pulverschicht aufgetragenen säurebeständigen, porösen Schicht (9) unbeweglich gemacht werden, und welche gas- und flüssigkeitsdurchlässig und für Teilchen der Pulverschicht undurchlässig ist; und
 - Schwefelsäure-Elektrolyten, mit denen die Plusplatte und die Minusplatte (1,2) sowie die Pulverschicht in einer zum Laden und Entladen der Batterie im wesentlichen erforderlichen und ausreichenden Menge getränkt und die in selbigen gehalten werden .
 - 35
14. Geschlossene Blei/Säure-Batterie nach Anspruch 13, wobei der zum Laden und Entladen der Batterie erforderliche Elektrolyt im wesentlichen von den feinen Primärteilchen in der Pulverschicht gehalten wird und wobei ein Sauerstoffgas, welches sich während des Ladens an der positiven Elektrode (1) entwickelt, durch die Gaskanäle hindurch von der Minusplatte (2) absorbiert wird, wobei die Batterie einen Sauerstoffkreislauf ohne freie Elektrolyte verwendet.
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15. Geschlossene Blei/Säure-Batterie nach Anspruch 14, wobei die als Elektrolyt-Haltelement genutzte Pulverschicht als einen Hauptbestandteil ein wasserhaltiges Siliziumdioxid ($\text{SiO}_2 \cdot n\text{H}_2\text{O}$) mit feinen Primärteilchen in einer Größe von 5 - 40 Millimikronen enthält, die sich zu Sekundärteilchen mit einer Größe von 10 - 500 Mikronen anhäufen und wobei die Pulverschicht eine spezifische Oberfläche von 100 - 400 m^2/g und eine Porosität von 85 - 90 % hat und mindestens 2 mg Antimon pro Gramm Pulver adsorbieren kann.
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16. Geschlossene Blei/Säure-Batterie nach Anspruch 13, wobei das Gitter der Plusplatte ein positives Gitter aus einer Bleilegierung mit 0,7 - 2,0 Masseprozent Antimon, 0,10 - 0,3 Masseprozent Arsen und 0,01 - 0,5 Masseprozent Zinn ist und das Gitter der Minusplatte ein negatives Gitter aus einer antimonfreien Bleilegierung mit 0,02 - 0,12 Masseprozent Kalzium und 0,001 - 0,5 Masseprozent Zinn ist.
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17. Geschlossene Blei/Säure-Batterie nach Anspruch 13, wobei der Plattenscheider ein synthetischer Plattenscheider mit geringem Widerstand, einer Dicke von 0,02 - 0,3 mm und einer Porosität von 70 - 80 % ist und eine Vielzahl kleiner zylindrischer oder linearer Vorsprünge auf einer Seite oder beiden Seiten aufweist.
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18. Geschlossene Blei/Säure-Batterie nach Anspruch 17, wobei die Vielzahl kleiner zylindrischer oder linearer Vorsprünge zum Blockieren der Poren im Plattenscheider nicht mehr als 1 % der Gesamtfläche des Plattenscheiders einnimmt.
- 5 19. Geschlossene Blei/Säure-Batterie nach Anspruch 17, wobei die kleinen zylindrischen oder linearen Vorsprünge aus einem säurebeständigen Heißschmelzharz bestehen.
20. Geschlossene Blei/Säure-Batterie nach Anspruch 13, wobei die Plusplatte mit einer Masse pastiert ist, die ein Gemisch aus einem bleihaltigen Oxidpulver und Bleimennige umfaßt und letzteres mindestens 20 Masseprozent des bleihaltigen Oxidpulvers ausmacht.
- 10 21. Geschlossene Blei/Säure-Batterie nach Anspruch 20, wobei die Plusplatte Bleidioxid umfaßt, welches aus einem Gemisch aus Bleimennige, verdünnter Schwefelsäure und einem bleihaltigem Oxidpulver besteht, und das Gemisch eine Paste bildet, welche auf ein positives Gitter aufgetragen wird, und die Plusplatte elektrochemisch ausgehärtet und gebildet wird.
- 15 22. Geschlossene Blei/Säure-Batterie nach Anspruch 13, wobei die poröse Schicht eine Platte aus Phenolharzschäum ist, die größer als eine Oberseite des Behälters ist und zur Schaffung offener Zellen in einem Verhältnis von 10 - 100 aufgeschäumt wurde, und die Platte gegen die Oberseite des Behälters gepreßt und in die einzelnen Zellen der Batterie eingedrückt wird, um die im Behälter verdichtete Pulverschicht unbeweglich zu machen.
- 20 23. Geschlossene Blei/Säure-Batterie nach Anspruch 31, wobei die poröse Schicht unter einem Entlüftungstopfen angebracht und das Entlüftungsventil über dem Stopfen angeordnet ist, um die im Behälter verdichtete Pulverschicht unbeweglich zu machen.
- 25 24. Geschlossene Blei/Säure-Batterie nach Anspruch 13, wobei die starren Platten an den Flächen der Behälteraußenwände parallel zu der Plusplatte und der Minusplatte im Behälter befestigt werden, wodurch eine Verformung der Wandflächen des Behälters verhindert wird.
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Revendications

- 35 1. Batterie acide-plomb étanche avec une soupape d'évent comprenant : un bac (5) recevant un élément assemblé comprenant
- au moins une plaque positive formée électrochimiquement (1) ayant une grille d'alliage exempt d'antimoine enrobée d'un matériau actif poreux;
 - au moins une plaque négative formée électrochimiquement (2) ayant une grille d'alliage de plomb exempt d'antimoine enrobée d'un matériau actif poreux, et un séparateur (3) inséré entre lesdites
 - 40 plaques positive et négative (1, 2), ledit séparateur (3) ayant une pluralité de projections (4, 4') sur l'une de ses faces ou sur les deux;
 - une couche de poudre placée entre lesdites plaques positive et négative (1, 2) et autour dudit élément assemblé, ladite couche de poudre étant composée d'une poudre tassée fortement (8), qui est résistante à l'acide et hydrophile et qui a une porosité supérieure et une surface spécifique plus grande
 - 45 que lesdits matériaux actifs, ladite couche de poudre ayant des interstices dans son intérieur et ils sont utilisés comme canaux gazeux, créés lorsqu'on tasse intimement des particules secondaires grossières formées par l'agglomération de particules primaires fines qu'on immobilise avec une couche poreuse résistante à l'acide (9) placée au-dessus de ladite couche de poudre, ladite couche poreuse étant perméable aux gaz et aux liquides, et imperméable aux particules de ladite couche de
 - 50 poudre ; et
 - de l'électrolyte acide sulfurique imprégné et retenu dans lesdites plaques positive et négative (1, 2) et dans ladite couche de poudre en une quantité sensiblement nécessaire et suffisante pour charger et décharger la batterie.
- 55 2. Batterie acide-plomb étanche selon la revendication 1, où l'électrolyte nécessaire pour charger et décharger la batterie est sensiblement retenu par lesdites particules primaires fines dans ladite couche de poudre et où le gaz oxygène développé à l'électrode positive (1) pendant la charge est absorbé dans lesdits canaux de gaz par l'électrode négative (2), ladite batterie utilisant un cycle d'oxygène ne mettant pas en

oeuvre de l'électrolyte libre.

3. Batterie acide-plomb étanche selon la revendication 2, où ladite couche de poudre utilisée comme fixateur d'électrolyte contient comme composant principal du dioxyde de silicium hydraté ($\text{SiO}_2 \cdot n\text{H}_2\text{O}$), qui comprend des particules primaires fines ayant une taille de 5 - 40 millimicrons, lesdites particules primaires étant agglomérées pour former des particules secondaires ayant une taille de 10 - 500 microns, ladite couche de poudre ayant une surface spécifique de 20 - 400 m^2/g et une porosité de 85 - 90 %.
4. Batterie acide-plomb étanche selon la revendication 1, où ladite plaque positive utilise une grille positive en alliage de plomb exempt d'antimoine contenant 0,02 - 0,12 % en poids de calcium, 0,20 - 1,0 % en poids d'étain et 0,001 - 0,01 % en poids d'aluminium et ladite plaque négative utilise une grille négative en alliage de plomb exempt d'antimoine contenant 0,02 - 0,1 % en poids de calcium et 0,001 - 0,5 % en poids d'étain.
5. Batterie acide-plomb étanche selon la revendication 1, où ledit séparateur est un séparateur synthétique à basse résistance d'une épaisseur de 0,02 - 0,3 mm et une porosité de 70 - 80 % et qui possède une pluralité de petites projections cylindriques ou linéaires sur l'une de ses faces ou sur les deux.
6. Batterie acide-plomb étanche selon la revendication 5, où ladite pluralité de petites projections cylindriques ou linéaires qui bloque les pores dans le séparateur n'occupe pas plus de 1 % de l'aire totale dudit séparateur.
7. Batterie acide-plomb étanche selon la revendication 5, où lesdites petites projections cylindriques ou linéaires sont en résine thermofusible résistant à l'acide.
8. Batterie acide-plomb étanche selon la revendication 1, où la plaque positive est enrobée de pâte préparée en mélangeant une poudre d'oxyde de plomb avec du minium en une quantité d'au moins 20 % en poids de la poudre d'oxyde de plomb.
9. Batterie acide-plomb étanche selon la revendication 8, où ladite plaque positive comprend du dioxyde de plomb formé d'un mélange de minium et d'acide sulfurique dilué et de poudre d'oxyde de plomb ajoutée au mélange contenant le dioxyde de plomb, ledit mélange étant sous forme d'une pâte qu'on applique sur une plaque positive, ladite plaque positive étant durcie et formée électrochimiquement.
10. Batterie acide-plomb étanche selon la revendication 1, où ladite couche poreuse est une plaque de résine phénolique expansée qui a une taille supérieure à la face totale du bac et qu'on a expansée à une proportion de 10 - 100 pour produire des cellules ouvertes, ladite plaque étant comprimée contre la face frontale du bac et introduite de force dans les cellules individuelles de la batterie pour immobiliser la couche de poudre tassée dans le bac.
11. Batterie acide-plomb étanche selon la revendication 1, où ladite couche poreuse est placée sous un tampon d'évent et la soupape d'évent est placée au-dessus dudit tampon d'évent pour immobiliser la couche de poudre tassée dans le bac.
12. Batterie acide-plomb étanche selon la revendication 1, où on fixe des plaques rigides aux surfaces de parois externes du bac parallèles aux plaques positive et négative dans le bac, ce qui empêche ainsi la déformation des surfaces de paroi externes du bac.
13. Batterie acide-plomb étanche qui a une soupape d'évent comprenant : un bac (5) recevant un élément assemblé comprenant:
 - au moins une plaque positive formée électrochimiquement (1) ayant une grille en alliage de plomb contenant une petite quantité d'antimoine, ladite plaque positive (1) étant enrobée d'un matériau actif poreux, et
 - au moins une plaque négative formée électrochimiquement (2) ayant une grille en alliage de plomb sans antimoine enrobée d'un matériau actif poreux, et
 - un séparateur (3) inséré entre lesdites plaques positive et négative (1, 2), qui a une pluralité de projections (4, 4') sur l'une de ses faces ou sur les deux faces;
 - une couche de poudre placée entre ladite plaque positive et ladite plaque négative (1, 2) et autour

- 5 dudit élément assemblé, ladite couche de poudre étant composée d'une poudre tassée fortement (8), qui est résistante à l'acide et hydrophile et qui a une plus grande porosité et une plus grande surface spécifique que lesdits matériaux actifs, ladite couche de poudre ayant des interstices en son intérieur qui servent de canaux de gaz, créés quand on forme des particules secondaires grossières par agglomération de particules primaires fines et qu'on tasse fortement et qui est immobilisée avec une couche poreuse résistant à l'acide (9) placée au-dessus de ladite couche de poudre, et qui est perméable aux gaz et aux liquides, et qui est imperméable aux particules de ladite couche de poudre ; et
- 10 - l'électrolyte acide sulfurique imprégné et retenu dans lesdites plaques négative et positive (1, 2) et dans ladite couche de poudre en une quantité sensiblement nécessaire et suffisante pour charger et décharger la batterie.
14. Batterie acide-plomb étanche selon la revendication 13, où l'électrolyte nécessaire à la charge et à la décharge de la batterie est sensiblement retenu par lesdites particules primaires fines dans lesdites couches de poudre, et où le gaz oxygène dégagé à l'électrode positive (1) pendant la charge, est absorbé dans lesdits canaux de gaz par la plaque négative (2), ladite batterie utilisant un cycle d'oxygène ne mettant pas en oeuvre de l'électrolyte libre.
15. Batterie acide-plomb étanche selon la revendication 14, où ladite poudre utilisée comme fixateur d'électrolyte contient comme composant principal du dioxyde de silicium hydraté ($\text{SiO}_2 \cdot n\text{H}_2\text{O}$) qui comprend des particules primaires ayant une taille de 5 - 40 millimicrons qui sont agglomérées pour former des particules secondaires ayant une taille de 10 - 500 microns, ladite couche de poudre ayant une surface spécifique de 100 - 400 m^2/g et une porosité de 85 - 90 % et qui est capable d'adsorber au moins 2 mg d'antimoine par gramme de ladite poudre.
16. Batterie acide-plomb étanche selon la revendication 13, où ladite grille de ladite plaque positive est une grille positive en alliage de plomb contenant 0,7 - 2,0 % en poids d'antimoine, 0,1 - 0,3 % en poids d'arsenic, 0,01 - 0,5 % en poids d'étain et ladite grille de ladite plaque négative est une grille négative en alliage de plomb sans antimoine contenant 0,02 - 0,12 % en poids de calcium et 0,001 - 0,5 % en poids d'étain.
17. Batterie acide-plomb étanche selon la revendication 13, où ledit séparateur est un séparateur synthétique à basse résistance qui a une épaisseur de 0,02 - 0,3 mm et une porosité de 70 - 80 % et qui contient une pluralité de petites projections cylindriques ou linéaires sur une de ses faces ou sur les deux.
18. Batterie acide-plomb étanche selon la revendication 17, où ladite pluralité de petites projections cylindriques ou linéaires qui bloquent les pores dans le séparateur n'occupent pas plus de 1 % de la surface totale dudit séparateur.
19. Batterie acide-plomb étanche selon la revendication 17, où lesdites petites projections cylindriques ou linéaires sont en résine thermofusible résistante à l'acide.
20. Batterie acide-plomb étanche selon la revendication 13, où la plaque positive est enrobée d'une pâte comprenant un mélange de poudre d'oxyde de plomb et de minium en une quantité d'au moins 20 % en poids de poudre d'oxyde de plomb.
21. Batterie acide-plomb étanche selon la revendication 20, où ladite plaque positive comprend du dioxyde de plomb formé d'un mélange de minium et d'acide sulfurique dilué et d'une poudre d'oxyde de plomb, ledit mélange formant une pâte qu'on applique sur une grille positive, ladite plaque étant durcie et formée électrochimiquement.
22. Batterie acide-plomb étanche selon la revendication 13, où ladite couche poreuse est une plaque de résine phénolique expansée qui a une taille supérieure à la face supérieure du bac et qui a été expansée en une proportion de 10 - 100 pour produire des cellules ouvertes, ladite plaque étant appliquée contre la face frontale du bac et introduite de force dans les cellules individuelles de la batterie pour immobiliser la couche de poudre tassée dans le bac.
23. Batterie acide-plomb étanche selon la revendication 13, où ladite couche poreuse est placée sous un tam-

pon d'évent et la soupape d'évent est placée au-dessus dudit tampon d'évent en vue d'immobiliser la couche de poudre tassée dans le bac.

- 5 **24.** Batterie acide-plomb étanche selon la revendication 13, où des plaques rigides sont fixées aux surfaces de paroi externe du bac parallèlement aux plaques positive et négative dans le bac, ce qui empêche la déformation desdites surfaces de paroi du bac.

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FIG. 1

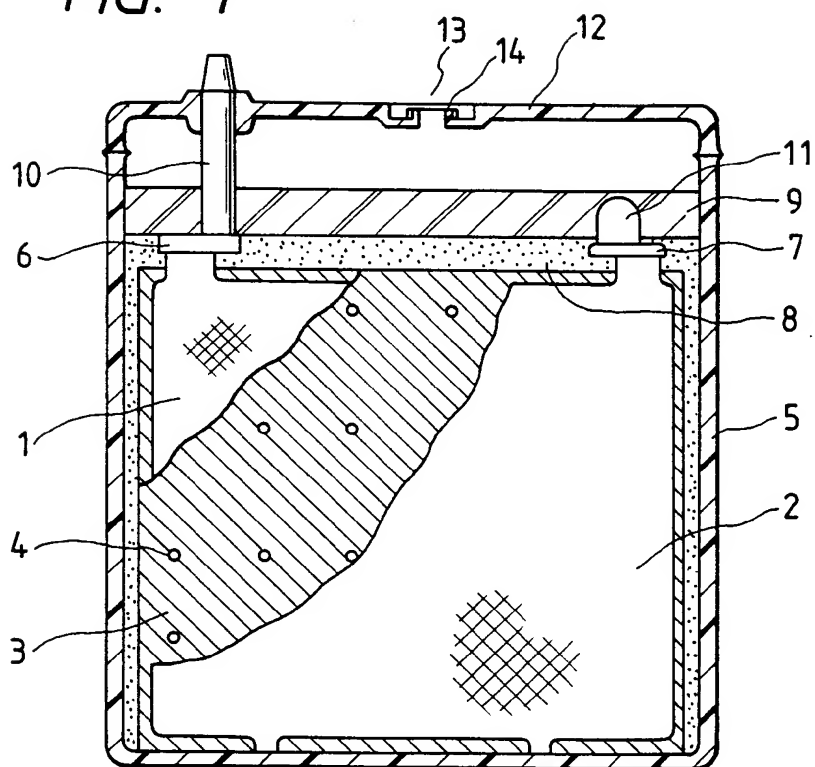


FIG. 2

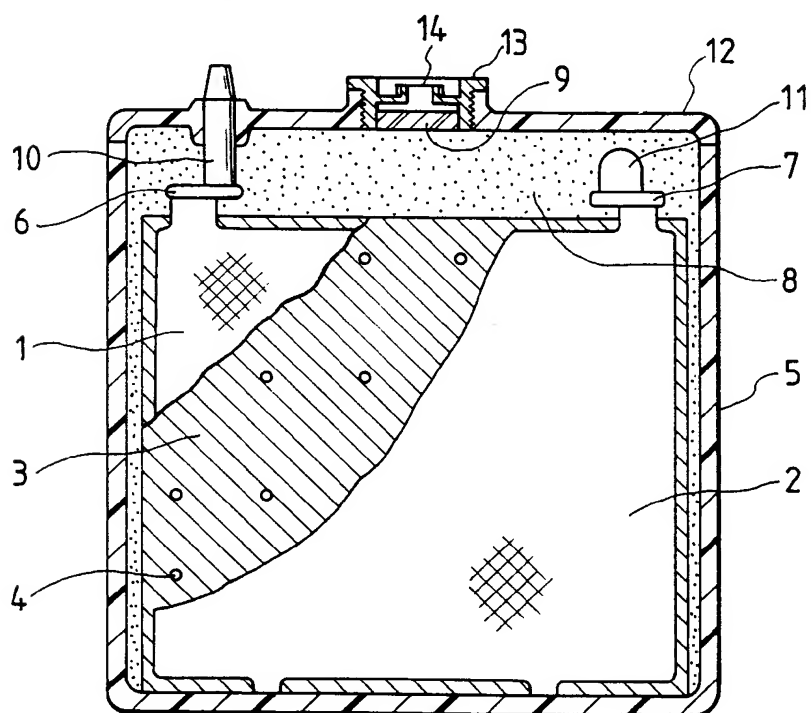


FIG. 3

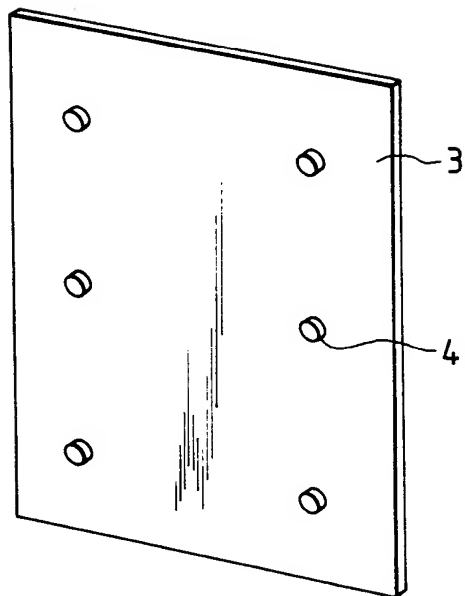


FIG. 4

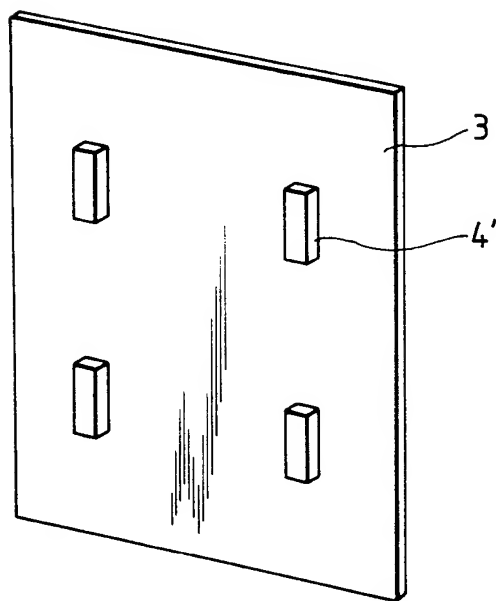


FIG. 5

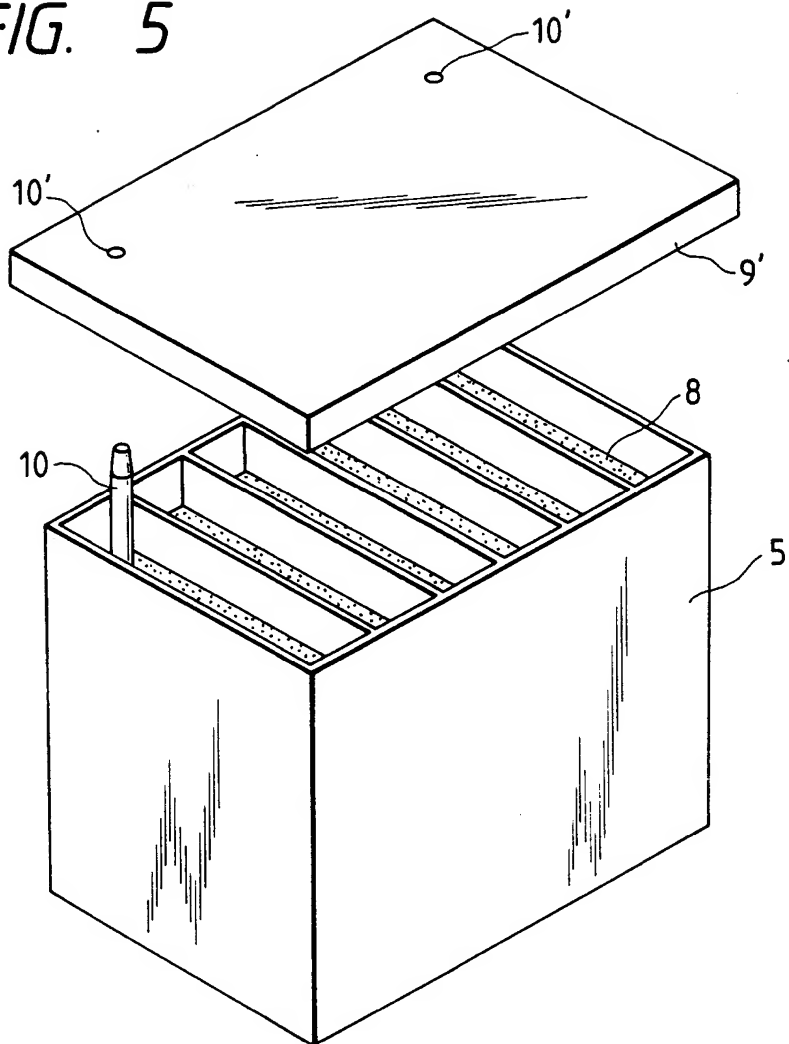


FIG. 6

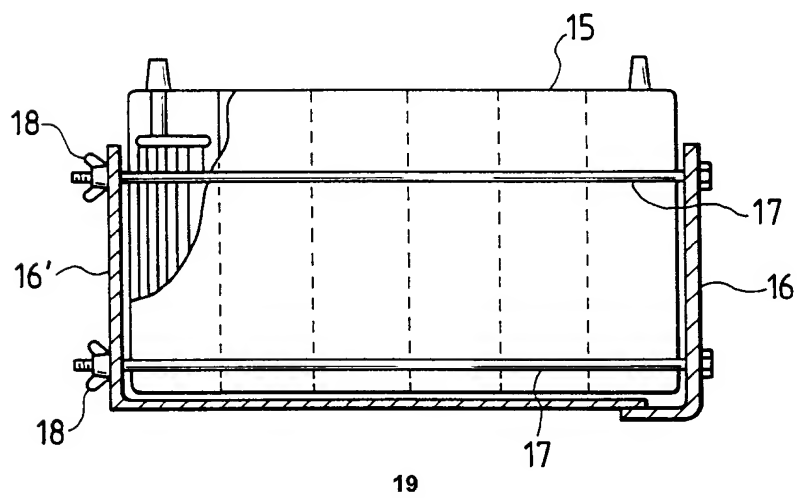


FIG. 7

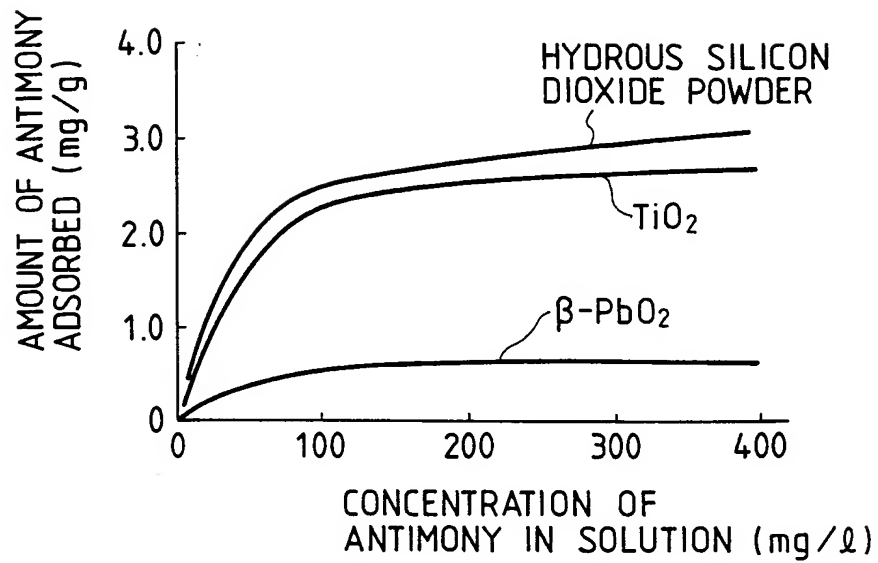


FIG. 8

